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CLAIM AMENDMENTS

- (Currently amended) A substantially two-phase hard 1. metal substrate body comprised consisting essentially of a WC hard material phase consisting of WC and a binder phase of 3 to 25 mass % which apart from at least one of the binder metals Fe, Co and/or Ni contains up to 15 mass % of the binder phase a dissolved dopant selected from the group comprised consisting of Al, Cr, V, Nb, Ta, Ti, Zr, and Hf, characterized in that wherein the percentage proportion of all doping agents dopants as a whole in the two-phase hard metal substrate body is limited to a maximum of 4 mass % in that ; wherein the proportion of a cubic phase consisting of said dopant in undissolved form in the two-phase hard metal substrate is less than 4 volume % and in that; wherein the binder metal content in a hard metal-substrate body boundary zone falls from up to 1 µm, preferably up to 0.5 µm to less than 0.5 times an edge zone of the two-phase hard metal substrate drops to less than half the binder metal content in the substrate body interior.
 - 2. (Currently amended) The <u>substantially</u> two-phase hard metal substrate body according to claim 1 characterized in that wherein the concentration of the <u>binder metal in the</u> binder phase falls gradually toward the substrate body surface and the concentration of the dopant <u>in the binder phase</u> gradually increases in a corresponding manner.

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3. (currently amended) The <u>substantially</u> two-phase hard metal substrate body according to claim 1 characterized in that

wherein the grain size of the WC is < 1.5 μm whereby the WC fine hard metal material phase (grain size < 0.8 μm) and/or with WC ultrafine grain hard metal material phase (grain size < 0.5 μm),

preferably contain Cr, V and/or Ta as dopant.

- 4. (Currently amended) The <u>substantially</u> two-phase hard metal substrate body according to claim 1 characterized in that wherein at lest one layer is applied to the substrate body surface, the layer being comprised of a carbide, nitride and/or carbonitride of Ti, Zr and/or Hf and/or of Al₂O₃, HfO₂, ZrO₂, oxides, amorphous carbon, diamond, cubic boron nitride, carbon nitride (CN_x) or another compound of at least one of the elements B, C, N and/or O.
- 5. (currently amended) The <u>substantially</u> two-phase hard metal substrate body according to claim 1 characterized in that wherein in the boundary zone close to the surface there is an enrichment with nitride or carbonitride of the metal dopant.
 - 6. (Withdrawn) A method of producing a two-phase hard metal substrate body according to claim 1 in which the starting mixture is preheated powder metallurgically is prepressed to a green body and then in an atmosphere of a furnace is heated and sintered, characterized in that in the heating phase, after reaching the eutectic, but no later than reaching the sintering

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- 7 temperature the vacuum or inert gas atmosphere is replaced with a
- 8 N_2 atmosphere with a N_2 pressure of $\leq 10^5$ Pa and is maintained at
- 9 least until the sintering temperature is reached.
- 1 7. (withdrawn) The method of making a two-phase hard 2 metal substrate body according to claim 1 in which the starting 3 mixture is powder metallurgically treated and is pressed to a green 4 body and finally heated in an atmosphere of a furnace and sintered, 5 characterized in that after finish sintering or optionally in a 6 final treatment above the eutectic temperature, the sintered body 7 is maintained in a N, atmosphere under a pressure (p) of 10^5 Pa < p < 107 Pa for at least 10 minutes. 8
- 8. (withdrawn) The method according to claim 6

 characterized in that the nitrogen atmosphere is established by

 introducing precursors that is N-containing gases whereby the

 nitrogen is formed in situ in the gas atmosphere.
 - 9. (withdrawn) The method according to claim 6 characterized in that the two-phase hard metal substrate body is heated up to 1250°C during the heating phase and this temperature is held for at least 20 minutes, preferably more than 1 hour, before the heating up is continued to the sintering temperature.

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- 10. (withdrawn) The method according to claim 6

 2 characterized in that initially in the heating up phase at about

 1200°C the previously existing vacuum is replaced by an inert gas

 4 atmosphere, preferably with a pressure of 10³ Pa to 10⁴ Pa and only

 5 upon reaching the sintering temperature is a nitrogen containing

 6 atmosphere established with a higher pressure, preferably > 10⁴ Pa.
- 1 11. (withdrawn) The method according to claim 6
 2 characterized in that the heating up rate and the cooling down rate
 3 amounts to up to 10°C/min, preferably between 2°C/min and 5°C/min.
 - 12. (withdrawn) The method according to claim 6 characterized in that the starting mixture contains in an amount of up to 15 mass % of the binder phase additional carbides, nitrides, carbonitrides of the elements of Group IVa or VIa of the periodic system or Al or complex carbides, complex nitrides and/or complex carbonitrides of the form Ti₂AlC, Ti₂AlN, Cr₂AlN, Cr₂AlC.